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(57) Abstract

A rechargeable battery such as a lithium ion battery is charged or discharged by supplying an electrical current to the battery or withdrawing electrical energy from the battery. In order to optimize the charging and/or discharging process the temperature of the battery can be increased during at least part of the charging and/or discharging process by reducing losses in heat-generated energy due to spontaneous heating of the battery during the charging and/or discharging process. The reduction in loss of energy can be obtained by having a layer of a heat-insulating material at least partly surrounding the battery. In order to increase the battery temperature heat-generated energy may be supplied to the battery in addition to the energy supplied to the battery by the charging current so as to maintain the outer temperature of the battery within a predetermined range during a major part of the charging process. The invention also relates to a voltage-balanced charging process wherein a battery comprising two or more cells is charged so that the voltage of each cell is about to reach the same maximum cell voltage. It is preferred that in the balanced charging process the voltage of each cell is determined at several points in time during charging, and that the charging current of each cell is controlled so as to maintain the voltage of each cell mainly equal during a major part of the charging process. The invention further relates to a battery system comprising a battery pack with one or more battery cells forming a rechargeable battery, where the battery pack comprises a layer of a heat-insulating material at least partly surrounding the battery during discharging or charging.

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A METHOD AND AN APPARATUS FOR CONTROLLING BATTERY TEMPERATURE DURING CHARGING/DISCHARGING

The present invention relates to controlling the temperature of a rechargeable battery during charging or discharging and, 5 more particularly, to optimize the charging or discharging process of such batteries. The invention also relates to a battery system for performing the method.

Rechargeable storage cells or batteries are electrochemical devices for storing and retaining an electrical charge and later delivering that charge as useful power. A battery may typically have a number of storage cells connected together to form a battery having specific voltage or current delivery capability. A familiar example of a rechargeable battery is the nickel-cadmium, NiCd, battery used in portable electronic devices such as cameras and mobile telephones. 15

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When charging a rechargeable battery, such as an NiCd battery, an electrical voltage greater than the terminal voltage of the battery may be applied to the terminals of the battery whereby a current will run through the battery. This current initiates a chemical process by which energy is stored in the battery.

Frequently, the charging period for a battery is desired to be as brief as possible, which has lead to the use of greater and greater charging currents. This may accelerate the heatgenerating process within the battery which again may cause chemical destruction of the battery, and therefore it is important to interrupt charging at the proper time. The art includes some methods which attempt to ensure optimum charging with high charging currents where the charging process is stopped at the proper time before the heat generation within the battery becomes too high. Such methods are described in WO 92/15142 and WO 94/05068.

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However, when charging a rechargeable battery at high current rates, it has been recognized that the temperature of the battery cells should be high enough to ensure that the chemical process, which converts the charging current to energy within the battery, will be able to react fast enough to allow a desired high charging current. Under normal circumstances, this is not a problem for NiCd batteries or cells although it has been found that for low battery temperatures, for example below 0 °C, the maximum allowed charging current should be reduced as when compared to charging at a higher battery temperature such as 25 °C.

However, for other types of rechargeable cells, it has been found that in order to allow a high charging current for a major part of the charging period and, thus, obtaining a 15 short charging period of time when charging a cell, the temperature of the battery cells should be increased above usual ambient temperature. Furthermore, it has been recognized that for such types or similar types of cells, the cells may dissipate heat during both charging and discharging. Thus, as the dissipated heat represents energy, the 20 discharging capacity of the cells may vary with the thermal dissipation of energy, which again may vary with the outer temperature of the cells during discharge. This type of cells may comprise lithium cells, such as lithium ion cells, which 25 for example may be LiCoO₂, LiNiO₂, Li₂Mn₂O₄, Li_xV₂O₅ and Li_xV₅O₁₃, and lithium polymer cells. The problem is thus to ensure an optimum battery or cell temperature during charging; likewise, there is also a problem in obtaining an optimum battery or cell temperature during discharging.

When charging a rechargeable battery cell such as a lithium cell, it is well known that it is very important to prevent overcharge of the individual cells within the battery. An overcharge-preventing device is described in EP 0 512 340. However, the system described in EP 0 512 340 terminates charging when one of the cells in a battery pack comprising several cells connected in series reaches a predetermined

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maximum cell voltage, which may be defined by the battery component materials and the battery design. Thus, as the individual cells may have different charging and discharging characteristics, not all cells will be charged to the same degree by the system disclosed in EP 0 512 340.

Therefore, there is a need for an improved overcharging device or system which balances the charging of the individual cells during charging. Such a charge-balancing system is disclosed in US 5,283,512. The system described in US 5,283,512 measures the voltage of each individual cell during charging, and when a cell has reached the predetermined maximum cell voltage, the charge current is by-passed around that cell.

However, neither EP 0 512 340 nor US 5,283,512 has any mentioning of controlling the cell temperature in order to maximize charging and discharging of the battery or cells. Thus, there is a need for an improved charge-balancing and overcharge-preventing method and system which may also control the temperature of the battery cells during charging and/or discharging.

The present invention provides a solution to the above mentioned problems.

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A solution is achieved according to the invention by a method of charging a rechargeable battery in which method energy is supplied to the battery by supplying an electrical current to the battery so as to charge the same. The supplied charging current may generate heat within the battery during the charging process, and this charging-generated heat may be sufficient to maintain the outer temperature of the battery within a predetermined range during a major part of the charging process. However, it is preferred to supply heat-generated energy to the battery in addition to the energy supplied to the battery by the charging current so as to maintain the outer temperature of the battery within the

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predetermined range during a major part of the charging process. Here, the battery may be a single battery cell or several battery cells if the battery is formed by several battery cells.

5 When the outer cell temperature is increased to a predetermined range by a method according to the present invention, it may be possible to supply a high charging current to the battery or cells for an increased amount of time, which amount of time may be a function of the outer cell temperature. Thus, a more efficient charging process and a shorter overall charging period may be achieved by controlling the outer battery or cell temperature to be within a pre-selected range.

It is preferred that the heat-generated energy is delivered to the battery so as to obtain an outer temperature of the battery within the predetermined range during the initial phase of the charging process or prior to initiating the charging process.

The methods of the invention are particularly relevant to

lithium batteries, such as a lithium ion batteries which may
comprise one or more lithium ion cells. For this type of
batteries, the outer cell temperature may be in the range of
30-60 °C, preferably 40-50 °C, and more preferred in the
range of 41-46 °C. It should be understood that the purpose
of maintaining a relatively high outer cell or battery temperature during the charging process is to be able to allow a
high charging current for a major part of the charging process and thus a shorter overall charging time.

If the battery comprises more than one cell, it is preferred that the temperature of the battery is controlled so that the outer temperature of each cell is maintained mainly at the same value during the charging process in order to match the charging of each cells.

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Preferred examples of battery packs are described in the discussion given in connection with the figures. Thus, it is preferred that the battery or cells is/are packed in a heat-insulated battery pack with heat-generating components arranged within the battery pack. The heating components may be the battery cell or cells themselves, but in addition heat-generated energy may be supplied by at least a part of a charging circuitry arranged within the battery pack or by at least part of a special-purpose heat-generating circuitry arranged within the battery pack.

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When a battery comprising more than one cell is charged according to the present invention, it is preferred that the battery is charged using a voltage-balanced charging process so that the voltage of each cell is about to reach the same maximum cell voltage. The voltage of each cell may be surveyed during the charging process, and it is preferred that when the voltage of a cell reaches a predetermined maximum cell voltage, the charging current to this cell is reduced and the charging process is controlled so that the cell voltage is maintained about the maximum cell voltage during the remaining charging period. The charging process may be continued until the cell is fully charged, however, it may also be preferred that the cell is only charged to a certain degree of it full capacity such as 60%, 70%, 80% or 90%.

It is preferred that the balanced charging process is controlled so that each cell is charged to about the same capacity or about the same degree of its full capacity, preferably each cell should be charged to its full capacity. The balanced charging may be controlled so that the surveyed or measured voltages of the cells are mainly equal to each other during a major part of the charging process; this part of the charging process may also include a first phase of the charging process where none of the cells have yet reached the maximum cell voltage. If the surveyed voltage of a first cell is increased above the surveyed voltage of a second cell, it is preferred that the first cell is being discharged for a

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period of time while the second cell is still being charged, so that after the discharging period of time, the two cells may be further charged at about the same cell voltage level.

The charging circuitry for controlling the balanced charging
may comprise more than one by-pass device in order to by-pass
the charging current for each individual cell, so that each
cell may be charged to the same degree of the cell capacity
without any overcharge of the cells. The by-pass devices may
comprise components which are heated by the by-passed current, and, thus, the heating of these components may also be
used in maintaining a predetermined outer cell temperature or
temperature interval. If one of the cells is discharged
during the charging process, the discharged current may also
be led through a sort of by-pass device, and this by-pass
device may be heated by the discharging current.

For some types of cells, the inner cell temperature increase is larger during discharging than during charging. Thus, the temperature within a battery pack and thereby the outer cell temperature may be controlled by having at least one dis-20 charging period for at least one cell during the charging period. In addition to the heat generated within the cells, heat generated within part of the charging circuitry arranged within the battery pack may also add to the external heating of the battery cells. As mentioned above, a special-purpose heat-generating circuitry may be arranged within the battery pack, and the heat-generating current supplied to this circuitry may be controlled so as to generate sufficient heat in order to maintain the predetermined outer cell temperature or temperature range if or when the heat dissipates from the cells and/or the charging circuitry is insufficient to maintain the desired outer cell temperature.

The present invention also relates to a method of discharging a rechargeable battery comprising the steps of withdrawing electrical energy from the battery for discharging the same, and supplying heat-generated energy to the battery or main-

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taining heat generated within the battery, so as to increase the outer temperature of the battery during at least part of the discharging process.

As heat may be generated within a battery or battery cell
during the discharging process, the thermal energy loss from
the battery cell may be minimized by having a heat-insulating
layer around at least part of the battery cell. In such a
case, the internal generated heat will cause the outer cell
temperature to rise due to the small thermal loss, and this
may be sufficient to obtain an improvement in the discharging
capacity of the cell as when compared to a cell without heat
insulation. Thus, at least part of the heat-generated energy
may be supplied by spontaneous heating or internal heating of
the battery during the discharging process.

15 If the battery cell is packed in a battery pack, which battery pack may just be a heat-insulating layer, the increase in the outer temperature of the battery may be obtained during at least part of the discharging process by feeding current from the battery to an electric circuitry or component arranged within the battery pack or between the battery cell and the heat-insulating layer, where said circuitry or component is heated by the supplied current.

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It is also preferred that an electric circuitry or component arranged within the battery pack or between the battery cell and the heat-insulating layer is heated by a current supplied from an external current source. This external current may be supplied during the discharging process, but it is preferred that the external current is supplied before the initiation of the discharging process so that the outer cell temperature may have reached a predetermined temperature range before the discharging process is started, whereby the discharging capacity of the battery cell may be improved.

The present invention furthermore provides a battery pack with one or more battery cells forming a rechargeable bat-

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tery, where the battery pack comprises a layer of a heatinsulating material at least partly surrounding the battery
so as to maintain within the battery pack at least part of
the energy generated by spontaneous heating or internal
heating of the battery during discharging or charging. This
battery pack may be part of a battery system. Preferably, the
battery pack further comprises a heat-conductive material
arranged between the battery cells and the heat-insulating
layer, which heat-conductive layer at least partly surrounds
the battery cell or cells.

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It is preferred that such a battery pack and/or system is used in one or more of the above-mentioned methods of charging and discharging. Thus, the battery pack or system may further comprise an electric circuitry or component adapted to supply electric energy in the form of current generated heat to the battery pack so as to increase the outer temperature of the battery cell or cells when said energy is supplied. It is also preferred that the electric circuitry comprises at least part of a battery charging system arranged within the battery pack. This part of the charging system may comprise one or more by-pass devices adapted to by-pass charging current supplied by the charging system to at least one battery cell during a charging process.

In addition to the by-pass devices, the electric circuitry

25 may further comprise at least one electric component, said
component being arranged within the battery pack and being
adapted to deliver current-generated heat to the battery pack
when the heat generated by the by-pass devices and/or by
spontaneous heating within the cells is insufficient to

30 maintain the outer temperature of the battery within a predetermined temperature range. It is preferred that the batterycharging system is adapted to by-pass the charging current
around one of the battery cells when a voltage measured
across said one battery cell is equal to or larger than a

35 preselected maximum cell voltage.

Embodiments and details of the system appear from the claims and the detailed discussion of embodiments of the system given in connection with the figures.

- The invention will now be described in further detail in connection with the drawing in which
 - Fig. 1 shows the charging curves for a lithium ion cell with an outer cell temperature in the range of 42 to 46 °C, Figs. 2 and 3 show the discharging curves for a cell charged according to the charging process of Fig. 1 with the outer
- 10 cell temperature in the range of 44 to 47 °C and 25 to 30 °C, respectively,
 - Fig. 4 shows the charging curves for the lithium ion cell of Fig. 1 with an outer cell temperature in the range of 4 to 11 °C,
- 15 Fig. 5 shows the discharging curves for a cell charged according to the charging process of Fig. 4 with the outer cell temperature in the range of 24 to 28 °C,
- Fig. 6 shows the charging curves for the lithium ion cell of Fig. 1 with an outer cell temperature in the range of 4 to 8 °C,
 - Fig. 7 shows the discharging curves for a cell charged according to the charging process of Fig. 6 with the outer cell temperature in the range of -1 to 4 °C,
- Fig. 8 shows the charging curves for the lithium ion cell of 25 Fig. 1 with an outer cell temperature in the range of 39 to 42 °C,
 - Fig. 9 shows the discharging curves for a cell charged according to the charging process of Fig. 8 with the outer cell temperature in the range of 1 to 17 °C,
- Figs. 10-12 show battery systems according to the invention, Figs. 13-19 show balanced charging systems for use in a method or a battery system according to the invention, Fig. 20 shows a flow chart diagram of a charging process according to the invention,
- 35 Fig. 21 shows a flow chart diagram of a discharging process according to the invention,

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Fig. 22 shows the discharging curves for an insulated lithium ion cell with an ambient temperature of -3°C,
Fig. 23 shows the discharging curves for a non-insulated lithium ion cell with an ambient temperature of -3°C, and
Fig. 24 shows the discharging curves for a non-insulated NiCd battery with an ambient temperature of -3°C.

Fig. 1 shows the charging curves for a lithium ion cell of the LiCoO2 type where the outer temperature of the cell is controlled so as to be in the range of 42 to 46 °C. The 10 charging process is controlled so that a nearly constant charging current of 950 mA is supplied to the cell until a predetermined maximum cell voltage Vmax is reached. This maximum voltage is given by the manufacturer of the battery cell to be 4,2 Volts. Here overcharge of the cell should be avoided in order to avoid damage of the cell. When Vmax is 15 reached, the charging process is controlled so that the charging current is decreased but the cell voltage is maintained around Vmax until termination of the charging process. In the example shown in Fig. 1, the charging process is 20 terminated after 40 minutes. A charging period of 40 minutes is also chosen for the following charging examples.

Figs. 2 and 3 show discharging curves for the charged cell of Fig. 1. In Figs. 2 and 3, the outer cell temperature is controlled to be in the range of 44 to 47 °C and 25 to 30 °C, respectively, the cell is discharged by an almost constant current of 425 mA, and the cell is discharged from a cell voltage of 3.88 Volts to a minimum cell voltage Vmin, which is given by the manufacturer of the battery cell to be 2.5 Volts. Overdischarge of the cell should be avoided in order to avoid damage of the cell. It should be noticed in this connection that the discharging time is approx. 94 minutes in Fig. 2 while the discharging time is lowered to approx. 90 minutes in Fig. 3 corresponding to a lowering in the cell capacity. As the cell has been charged to the same degree in both cases, the difference in cell capacity might be

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explained by the difference in the outer cell temperature during discharging.

As the lithium cell itself is expected to generate heat within the cell during the discharging process, this selfgenerated heating also being called spontaneous heating, a difference in outer cell temperature will correspond to a difference in temperature gradients within the cell, and, thus, to a difference in thermal-energy dissipation during the discharging process. If a part of the stored chemical energy is lost as heat, a smaller part of the chemical energy is left to be converted to electrical energy, resulting in a lowering of the cell capacity.

Fig. 4 shows the charging curves for the lithium ion cell of Fig. 1 when the outer cell temperature is controlled so as to be in the range of 4 to 11 °C. Here, the maximum charging current of 950 mA is only supplied to the cell for a relatively short period of time as Vmax of 4.2 Volts is reached rather quickly as when compared to the charging curves of Fig. 1. Thus, when the outer cell temperature is lowered during charging, the maximum cell voltage may be reached at an early stage in the charging process resulting in a lowering of the charging voltage and a lowering in the supplied energy to the cell. The cell charged in accordance with Fig. 4 should therefore be charged to a lower degree of its full capacity than when charged in accordance with Fig. 1.

This is illustrated in Fig. 5 which shows the discharging curves for a cell charged according to the charging process of Fig. 4. In Fig. 5, the outer cell temperature is controlled so as to be in the range of 24 to 28 °C, corresponding to the discharge process shown in Fig. 3. When comparing the curves of Figs. 3 and 5, the minimum cell voltage is reached after 68 minutes in Fig. 5 compared to 90 minutes in Fig. 3, and it is clearly illustrated that the cell has not been charged to the same degree by the process of Fig. 4 as when charged according to the process of Fig. 1.

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Fig. 6 shows the charging curves for a charging process similar to the process shown in Fig. 4, and Fig. 7 shows the discharging curves for a cell charged according to the charging process of Fig. 6. In Fig. 7, the outer cell temperature is controlled so as to be in the range of -1 to 4 °C, which is much lower than the temperature range of the discharging curves of Fig. 5. When comparing the curves of Figs. 5 and 7, the discharging time of Fig. 7 is 45 minutes whereas it is 68 minutes in Fig. 5. Thus, a significant reduction in the cell capacity is observed when the cell temperature is lowered about 25 °C during discharging.

Fig. 8 shows the charging curves for a charging process similar to the process of Fig. 1, and Fig. 9 shows the discharging curves for a cell charged according to the charging 15 process of Fig. 8. In Fig. 9, there is no controlling of the outer cell temperature, but the cell is packed in a heatinsulated battery package and cooled to a temperature around 1 °C before the discharging process is started. The temperature increase observed in Fig. 9 is due to the self-generated heating of the cell. When compared to Fig. 3 the capacity has 20 been lowered a bit from 90 minutes to 87 minutes, showing that an efficient heat insulation of the cell might reduce the loss of self-generated heat from the cell, and the generated heat will be used to warm up the battery cell, which again may result in an increased discharging cell capacity.

Preferred embodiments of a heat-insulated battery system according to the invention are shown in Figs. 10, 10A, 11, 11A and 12. In these embodiments a battery pack 100 comprises one or several battery cells 101, which may be at least partly surrounded by a heat-conductive layer 102. It is also preferred that the cells and/or the heat-conductive layer are/is at least partly surrounded by a heat-insulating layer 103 in order to prevent heat dissipation from the battery pack. In order to control the temperature of the heat conductive layer and/or the outer temperature of the cells, one or more heating components 104 may be arranged in the battery

pack. The heating components may preferably be resistors which may be arranged on the heat-conductive layer 102. The heat-conductive layer 102 may alternatively also be designed as a heating component itself. In order to control the outer temperature of the cell or cells, a temperature sensor is preferably arranged within the battery pack. Here it is preferred that the temperature sensor is arranged so as to measure the outer temperature of one or more cells and/or the temperature of the heat conductive layer.

- In order to control the outer cell temperature or in order to 10 supply current to a heating component or circuitry 104 during a charging or discharging process, the battery system should also include a current-supplying system; the current-supplying system may in a preferred embodiment comprise a control circuit for determining the outer cell temperature by measur-15 ing this temperature and controlling the current delivered to the heat dissipating component or components by the currentsupplying system. Such a control circuit or system may be included in the battery pack 100 (Figs. 11 and 11A). Electric 20 circuitry or components included in the battery may be arranged on a flexible printed circuit board 105, which may be of a heat-conductive material and may be arranged in close connection with the battery cell or cells and/or the heat conductive layer 102.
- In Fig. 12 is shown a preferred embodiment of a battery pack, wherein a part 106 of the battery pack may be removed from the battery pack when the battery is used or inserted within a heat-generating device or apparatus such as a computer. Thus, when the part 106 is removed, heat may be supplied from outside the battery pack and help maintaining a high outer cell temperature. If preferred, it may also be possible to cool the battery cells when the part 106 is removed if the outer cell temperature is too high.

It is also preferred that a layer of a heat-reflecting material is included in the battery packs of Figs. 10-12 and at least partly surrounding the cells.

When several cells are included in a battery, the cells are 5 usually connected in series in order to obtain a high resulting battery voltage. However, the cells within the battery may have different characteristics; for example, the storage capacity as well as the internal resistance may vary for different cells. This may have the result that when charging a series connection of cells until a maximum battery voltage is reached, some of the cells having a high capacity will not be fully charged while cells having a low capacity might be overcharged. Furthermore, a cell which is not charged to the same degree as other cells within the series connection may be overdischarged and thereby damaged during discharging of the battery. Thus, subsequent overcharging and overdischarging of the battery cells may result in a degradation in the total battery capacity and further result in a shorter lifetime of the battery.

One way to achieve a battery having a long lifetime would be to select the individual cells so that each cell within the battery would have the same cell capacity. However, this is not very practical and the solution according to the present invention is to connect an electric circuitry to the battery, which circuitry should be able to ensure that the individual cells are charged to about the same degree without being overcharged. Furthermore, if the individual cells within a battery pack are all fully charged or all charged to about the same degree of the full capacity, each cell will mainly follow the same voltage curve during the following discharge procedure. Thus, if the cells are charged by a balanced charging system, overcharge should be avoided but also overdischarge may be avoided.

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Figs. 13-18 show examples of such balanced charging systems to be used in a method or a battery system according to the invention.

The charging system shown Fig. 13 is arranged within the battery pack and may be included on the flexible printed circuit board 105. In Fig. 13 the battery comprises 2 cells, 1301 and 1302, two control modules, 1303 and 1304, two reference voltage devices, 1305 and 1306, and two by-pass devices, 1307 and 1308. The external power supply is connected to 10 voltage inputs 1309 and 1310. During a charging process the control module 1303 compares the voltage of the cell 1301 with a predetermined reference voltage refV1, and when refV1 is reached, the control module regulates the by-pass device 1307 so that part of the charging current to the cell 1301 is lead through the by-pass device 1307. It is preferred that 15 the by-passed current is controlled so that the charging voltage of the cell 1301 is maintained at refV1 once refV1 has been reached. It is furthermore preferred that once refV1 has been reached, the charging process is terminated after a period of time, which may be a function of the time consumed from initiating the charging procedure to the point in time at which the cell voltage is about to be equal to refV1. The control module 1304 will follow the charging procedure described above for the cell 1302 with reference to a voltage 25 refV2.

It is preferred that the voltage refV1 is the same as the voltage refV2. The by-pass devices may for example be transistors. The control modules 1303 and 1304 may comprise analog circuitry but may also comprise a microprocessor.

When controlling a balanced charging, it may be preferred to control the charging of each cell in response to another characteristic charging parameter than the above-mentioned cell voltage. Thus, a charging parameter such as the energy supplied to the cell may be determined and used in order to obtain a balanced charging of the individual cells.

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Fig. 14 shows the same charging system as shown in Fig. 13, but here the charging system is not included in the battery pack. Thus, the battery pack should have connections, 1401-1403, to each of the cells to be matched with connections, 1404-1406, of the charging system, so that the voltage can be measured for each individual cell during charging.

Fig. 15 shows a balanced charging system similar to that of Fig. 13. However, the control modules, 1303 and 1304, and the voltage reference devices, 1305 and 1306, are replaced by a microcontroller or a microprocessor, 1501, connected to an oscillator, 1502. In the system of Fig. 15, the predetermined reference voltage or voltages may be stored within the controller, and the voltage of each cell may be measured by use of analog to digital converters, such as A/D1 and A/D2, within the controller 1501.

Fig. 16 shows a preferred embodiment of a balanced charging system similar to that of Fig. 15, but further including heat-dissipating components such as a resistor R1, 1601, corresponding to the components 104 described above in connection with Figs. 10-12. The current through the resistor 20 R1, 1601, may be controlled by the microcontroller 1501 through a current-limiting device such as a transistor Q4, 1602. The current through the heating component or components 1601 should preferably be controlled in response to the output from a temperature sensor, which respond to the outer 25 temperature of the cell or cells and inputs a temperature signal to the control device 1501. The controller 1501 may be preprogrammed to respond to the input from the temperature sensor so as to regulate the heat-generating current through the heating component or components in order to obtain a temperature within a predetermined temperature range. The outer cell temperature may be controlled both in a charging process and a discharging process. However, the predetermined temperature or temperature range may be different for the charging process and the discharging process.

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When charging the cells within the battery pack, heat may be generated within the cell or cells corresponding to a spontaneous heating of the cell or cells and may thus cause an increase in the outer cell temperature. When one of the cells reaches the predetermined maximum cell voltage, the charging current is preferably decreased through this cell, and the spontaneous heating delivered from this cell will decrease. Thus, in a preferred charging process, the battery cell or cells is/are heated before the charging process and/or during the initial phase of the charging process by current supplied 10 to the heating components such as a resistor R1, 1601, while the current supplied to the heating component or components is decreased as the heat generated within the cells and/or the charging circuitry during the charging process will be able to maintain the outer cell temperature within the 15 desired temperature range; when the charging current supplied to the cell or cells is decreased during the end of the charging process, the current supplied to the heating component or components such as resistor R1, 1601, is preferably increased accordingly in order to maintain the outer cell 20 temperature within the desired temperature range.

Yet another preferred embodiment of a balanced charging circuit or system is shown in Fig. 17. The charging system of Fig. 17 comprises a switch element 1703, which may be a transistor Q3, to interrupt the series connection between the 25 cells 1301 and 1302 during charging. The switch element 1703 is controlled by the control circuit 1501, and the charging current supplied to the cell 1302 is regulated by a regulating circuitry 1706 which may comprise a resistor 1704 and a transistor Q1, 1701. The current may be controlled by measur-30 ing the voltage of resistor 1704 while at the same time measuring the voltage across the cell 1302; the voltages may be measured by using analog to digital converters forming part of the control circuit 1501. The current supplied to cell 1301 is controlled in the same way as the current to 35 cell 1302 by use of a regulating circuitry 1707 which may comprise a resistor 1705 and transistor Q2, 1702. When the

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battery is operated in the discharging mode, the cells 1301 and 1302 are connected in series through the switch element 1703. When the cells are charged, the resistors 1704 and 1705 may be heated by the charging current and thereby dissipate heat to the battery pack.

In Fig. 17 each cell is charged individually, and it is possible for the control circuit 1501 to charge a first cell while at the same time discharging a second cell which second cell may have reached a higher charging voltage than the first cell. Thus, when discharging the second cell, the cell 10 voltage of the second cell may be brought to approx. the same level as the first cell. After discharging, the second cell may be charged further and the first cell may also be charged further; the discharged cell may generate internal heat during discharging and thus contribute to maintain a desired 15 temperature range of the outer cell temperature; the discharged current from the second cell may also generate heat in a by-pass device or a current regulating circuitry, 1706 or 1707. Fig. 18 shows the same balanced charging system as 20 shown in Fig. 17 but with the heating circuitry described above, which may comprise the components 1601 and 1602, being included in charging system.

Fig. 19 also shows a preferred embodiment of a balanced charging system. The system of Fig. 19 is very much similar to those of Figs. 15 and 16, but in Fig. 19 it is illustrated how heating elements or components may be placed both within the battery pack and outside the battery pack. In Fig. 19 the charging system comprises a battery pack 1901 and an external package 1902 for supplying charging power and heat during the battery charging process. External package 1902 comprises power electronics and a microprocessor 1904 and a heating element 1905 which may be a heat-dissipating resistor.

During the charging process and/or prior to the charging process, the battery pack is heated by external heating element 1905. A temperature sensor 1906 is placed within

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battery pack 1901 and outputs a signal to processor 1904 in the external package. This signal is used by processor 1904 in order to control the power supplied to heating element 1905 and thereby the heat which is delivered to battery pack 5 1901. The heat delivered by heating element 1905 should be controlled so that the temperature of battery cells 1301 and 1302 within battery pack 1901 is kept within a predetermined temperature range during a major part of the charging process. The balanced charging process is controlled by processor 1501 as described previously in connection with Figs. 13 10 and 15. However, while charging battery cells 1301 and 1302, heat may also by delivered to the battery pack from internal heating element 1903 and from spontaneous heating of the cells thereby reducing the amount of heat generated energy needed from external heating element 1905. 15

When discharging the battery cells of Fig. 19 it may be desired to maintain the outer cell temperature of the cells within a predetermined temperature range. This desired cell temperature may be obtained by spontaneous heating of the cells during discharging, but it is preferred to speed up the temperature increasing process by drawing power from the battery cells and delivering this power to internal heating element 1903 during the discharging process. The amount of energy delivered by element 1903 is controlled by processor 1501 in response to input signals from temperature sensor 1906.

In general, microcontroller 1501 includes user programmable read only memory that contains a sequence of instructions that define the operation of the charging system. Referring to Fig. 20, when charging process 2000 is initiated, i.e. upon power up, after the hardware (e.g., counters and variables) are initialized (step 2002), a determination is made as to whether or not a proper battery has been inserted in the charger (step 2904). For example, the battery pack may include indicia of the type of battery to ensure that the battery pack is not inserted in an incompatible charger.

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Where the battery pack includes a microprocessor, a code word is provided to the charger apparatus upon inquiry. Assuming that an appropriate battery is coupled to the charger, voltage and various other information (such as temperature) is acquired (step 2006) and tested against criteria corresponding to the particular type of battery to ensure that the battery is in a condition for charging. For example, if the battery is below a certain voltage level, it may be indicative of damaged cells, and unsuitable for charging. Likewise, if the battery temperature is outside of a predetermined broad range, it may be inappropriate to effect a charge in process.

Assuming that conditions were not indicated as unsuitable, charging is then initiated (step 2010). In general, the

15 magnitude of the charging current is controlled according to measured parameters. Suitable charging current control is described in co-pending applications U.S. patent application serial no. 08/104,123 and WO 94/05068.

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Once the charging process has been initiated, the voltage of the respective cells and temperature are acquired and stored 20 in memory (step 2012) and checked against the predetermined limits (step 2014). Assuming that operation is still within limits, the voltage of each cell is measured, while measuring the voltage across resistor 1704, and are again measured and 25 stored in memory (step 2016). A balancing among the cells is then effected. The lowest cell voltage among the cells is then determined (step 2018). Bypass transistors (1701, 1702) are actuated for the cells with higher voltages to effectively equalize the charging (step 2020). Bypass current is then 30 measured for each of the cells (step 2022) to build an archival record, and the bypass current, and other data stored in memory for future use (step 2024).

Appropriate adjustments are then made to the heater (step 2026). The temperature of the cells is compared against

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indicia of desired temperature, and a current path through the heating element actuated or deactuated accordingly.

The various interval timers and the like associated with the charging current level are then updated (step 2028) and tested against conditions indicative of completion of the charging process (step 2030). Assuming that the charging process has not completed, steps 2012 through 2030 are the repeated.

Once charging is completed, the charger enters into what is in effect a wake state until the battery is removed (step 2032).

Referring to Fig. 21, microprocessor 1501 controls heating element 1903 and bypass devices 1307 and 1308 to maintain the temperature within a predetermined range, and ensure that overdischarge damage of the individual cells does not occur. Referring to Fig 21, when a discharge process is initiated, the voltage of the individual cells and temperature of the battery pack and any other relative characteristics are acquired, i.e., the respective A to D inputs of the microcontroller are read (step 2102).

The minimum voltage among the cells is then determined (step 2104), and the minimum voltage is then tested against a predetermined minimum threshold voltage (MinAllowedVolt) (step 2106). If the minimum cell voltage drops below the threshold value, the battery pack is effectively disconnected from the load (step 2108). Assuming that the minimum voltage is at least equal to the threshold value, the load is enabled (step 2110).

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The optimum discharge temperature is then determined (step 2112) and the heater adjusted accordingly (step 2114). During the charging operation, an external source of power is available. During battery discharge, however, the battery itself is the sole source of power, and the amount of power diverted

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to maintaining temperature becomes a concern, and it is desirable to determine the optimum temperature range, i.e. minimum temperature for maximum capacity. Such determination tends to be both battery and installation specific, but in 5 general, would be a formula based upon various constants pertaining to such things as the nature of the battery and application in which it is used, the discharge state of the battery, and ambient temperature. Once the optimum temperature is determined, power is provided to heater 1903 accordingly.

Discharge current is then measured (step 2116) and stored, together with other measured data for subsequent use (step 2118). The discharge sequence is then repeated.

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It should be understood that the above-described examples of Figs. 13-19 refer to battery charging systems which, prefer-15 ably, are used in order to obtain a fast charging process for battery cells, such as Lithium cells, by applying a high cell temperature during charging, whereby a high charging current is allowed for a major part of the charging process resulting in a short overall period of charging or recharging. Prefer-20 ably, the charging system of the present invention does not actuate any uncontrolled discharge of the battery cells while the battery is inserted in the power supplying unit.

It is further to be understood that during discharge of a battery cell in accordance with various aspects of the present invention, the cell is preferably heated by use of its own stored energy, since an external energy source may not be available. By using stored battery energy, when heating the battery cell or cells, it is made possible to use the battery at much lower ambient temperatures. For applications that draw high current pulses out of the battery (radio transmitters etc.), this solution might represent the only possibility for using the application at all at rather low temperatures.

As mentioned above, the predetermined temperature range may be different for the charging process and the discharging process, but preferably the minimum temperature of the battery cell should be determined so as to meet a set of cell parameters, such as internal impedance, useable capacity, lifetime etc. If the outer temperature of a battery cell is below such a minimum temperature, the battery cells are heated to reach this minimum temperature preferably before any charging is initiated.

10 Further, by using a balanced charging process, each of the battery cells may be charged in an optimal way, whereby the useable cycle life of the battery is prolonged.

Although the above-described examples of Figs. 13-19 refer to battery charging system for charging batteries comprising 2 cells, the principles of these charging systems may be extended to charging systems for charging batteries with more than 2 cells such a 3, 4, 5, 6 or more cells. Also, from the particular embodiments of the invention described above, various modifications may be made without departing from the spirit and scope of the present invention.

It should be understood from the above discussion that the battery cell temperature is a parameter which can have a major effect on the charging and discharging characteristics of the battery cell. However, the effects of changes in the battery cell temperature varies for different types of batteries.

This is further described in the following which gives a discussion on rechargeable cells based on solid state insertion, so-called guest-host systems:

This discussion points out the difference between well known types of rechargeable battery cells, such as Lead Acid and Nickel Cadmium cells, and the newer Insertion based types of cells, such a Lithium Ion cells.

The subject will be treated with attention to the effect of temperature on charge and discharge acceptance rates, as well as the effects of over charge and over discharge on net cell capacity.

5 For Nickel Cadmium and Lead Acid cells ion transport takes place in an aqueous solution with a high ionic conductivity.

Insertion (swing) battery cells are quite new, innovative secondary rechargeable battery systems, of which the Carbon/Lithium Cobaltite Intercalation system is an example. The term "Insertion" refers broadly to the introduction of a guest atom or molecule, ionized or neutral, into a host matrix. A redox process may be associated with the process. Thus, the redox process may take place, but it is not required to happen.

15 The Carbon/Lithium Cobaltite cell has a host with a layered structure for negative and positive plates, and the Lithium Ion will intercalculate in both.

The Lithium Ion is transported between the plates (and through a separator) by a ionconductive substance, which may be liquid or solid. It is generally recognized that in most Lithium cells, a Solid Electrolyte Interphase (SEI) is formed on the surface on the negative plate by reaction of Lithium with the electrolyte. The Lithium Ion must pass this surface film.

- The negative plate may be carbon (or a transition metal chalcogenide, halide, Bi, etc.). One example is Graphite, a Carbon allotrope that forms a layered structure with macromolecular sheets, consisting of hexagonal units of aromatic character, with good electron mobility.
- 30 Lithium Ions intercalate in the vacant Van der Wall sites between layers, giving the stoichmetric relation LiC_6 . In practice, the thin film Graphite plate may consist of short

range ordered domains, jumbled between each other. This, like the SEI film, may create bottlenecks with respect to Lithium Ion transport.

An other example of negative plate Carbon is Coke, a general term meaning a less ordered or amorphous structure, usually made by thermal decomposition of an organic substance.

The positive plate may by a metal chalcogenide, halide, $NiPS_3$ or other. Lithium Ion transport takes place in the lattice of the positive plate. Ion conduction varies according to material, structure and impurities.

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Choice of electrolyte is generally limited to aprotic compounds, stable towards the electrodes. Due to these considerations, the electrolyte often has limited ionic conductivity.

In general, ion transport in systems like Carbon/Lithium Cobaltite is temperature dependent, with conductivity/-transport increasing with temperature. The limiting factor is the electrolyte;

The problems of the electrolyte is compounded at low tem20 peratures. Temperature dependence of common electrolytes is
adequately described by the Arrehnius relation down to about
12 °C. At lower temperatures, the deviation is profound.

Ionic conductance in solids is temperature dependent, with a general increase in conductance as temperature is raised from room temperature level. This is the case with both plates in Lithium Cobaltite.

This means that low temperature poses a special problem to Lithium Ion cells. Insulating and/or heating the cell(s) can make a useless cell useful (that is, the effect of heating in this temperature range can be qualitative rather than quantitative). Typical temperature range is 15-10 °C and downwards.

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At higher temperatures, the relationship is linear, and insulating and/or heating the cell(s) can make it possible to charge the cell somewhat faster.

Nickel Cadmium and Lead Acid cells show prolonged charge time and/or reduced discharge rate at low temperatures, 0 °C and downwards, but the principal difference lies in the aqueous electrolyte with the established higher conduction rate of hydroxyl- and hydroxoniumion. In addition, salts typically have higher solubility in aqueous solution.

10 Overall, charge - and discharge acceptance rates are improved in Lithium Cobaltite swing cells as temperature is raised.

Temperature rise is limited, at some point, by instability of the electrolyte.

The observed effect of over charge is irreversible loss of
capacity, which in turn is thought to be due to structural
changes in the positive plate. Balancing of cell voltage in a
battery during charge ensures against loss of capacity.
Balancing can be active (all cells are charged to full capacity), or passive (battery charge stops when the first cell
reach its limit).

In summation, the differences in the physical conditions between established, commercial cells such as Nickel Cadmium and Lead Acid, etc., and Lithium Ion Cobaltite swing cells in terms of thermal behaviour is:

- 1. A substantially greater portion of ion conductance takes place in solids in a Lithium Ion Cobaltite cell as compared to a Nickel Cadmium or Lead Acid cell, which effects charge/discharge acceptance.
- 2. The electrolyte used in a Lithium Ion Cobaltite cell is
 non-aqueous resulting in a lesser ion conductivity at a given
 temperature as compared to the aqueous electrolyte used in a
 Nickel Cadmium or Lead Acid cell. Thus, the conductivity of a

Lithium Ion Cobaltite cell will have a less favourable temperature dependency than the conductivity of a Nickel Cadmium or Lead Acid cell.

Thus, due to the differences in the physical conditions of
Lithium Ion cells and well known types of cells such as
Nickel Cadmium or Lead Acid, the actual level of cell temperature during charging and/or discharging may have a much more fundamental effect on the operation of Lithium Ion cells than on the operation of Nickel Cadmium or Lead Acid cells.

Especially, when operating at low cell temperatures, for example below 10°C, below 0°C or below -5°C, a strong fall in the conductivity of Lithium Ion cells may be observed, which might lead to the result that the cell may not be used, since it will not be able to deliver a required discharging current at such temperatures.

The above mentioned differences of the effect of cell temperature during discharging is illustrated in Figs. 22-24 for a Lithium Ion cells and a NiCd battery.

Fig. 22 shows the discharging curves for an insulated lithium ion cell with an ambient temperature of -3°C. The type of cell is a Sony Ø18x65, Li-Ion cell, and the cell is discharged for about 3 minutes with a discharging current of 1,5 mA. During the discharging period the cell voltage decreases from 3,2 Volts to 2,5 Volts, which is the minimum operating voltage specified by the battery supplier.

Fig. 23 shows the discharging curves for the same Sony cell as shown in Fig. 22, but without insulation. Again, the ambient temperature is around -3°C, and the cell is discharged for about 3 minutes with a discharging current of 1,5 mA. During the discharging period the cell voltage decreases from 3,0 Volts to 2,5 Volts within a time period of about 2 minutes; from this point in time, the cell voltage is reduced rather drastically and reaches 1,5 Volts at the end of the 3 minutes. Thus, this cell will only be operating at an ambient

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temperature of -3°C for about 2 minutes, whereas the insulated cell will be operating for about 3 minutes due to the self generated heating of the insulated cell.

From the above discussion, it is to be expected that a NiCd battery should not show the same drastic reduction in operating time due to a low ambient temperature. This is illustrated in Fig. 24, which shows the discharging curves for a non-insulated NiCd battery with an ambient temperature of -3°C. Again, the cell is discharged for about 3 minutes with a discharging current of 1,5 mA. In order to compare the NiCd battery with the lithium cell of Fig. 23, the NiCd battery comprises 3 cells of the type Panasonic NiCd P70AAs, and, as can be seen from Fig. 24, the voltage drop which is dropped from 3,7 Volts to 3,35 Volts during the discharging period does not take the same drastic form as the voltage curve of Fig. 23.

Hence, the suggested methods and systems of the present invention provide solutions to the above mentioned problem by allowing the cell temperature of a Lithium Ion cell to be increased above the surrounding temperature value. This temperature increase may be provided in a controlled manner or may be provided by at least partly insulating the battery cell, as for example shown in the above described embodiments.

CLAIMS

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1. A method of charging a rechargeable battery comprising the steps of

supplying energy to the battery by supplying an electrical current to the battery so as to charge the same, and
supplying heat-generated energy to the battery in addition to the energy supplied to the battery by the charging
current so as to maintain the outer temperature of the battery within a predetermined range during a major part of the
charging process.

2. A method of charging a rechargeable lithium ion battery comprising the steps of

supplying energy to the battery by supplying an electrical current to the battery so as to charge the same, and increasing the temperature of the battery during at least part of the charging process by reducing losses in heat-generated energy due to spontaneous heating of the battery during the charging process, said reduction in loss of energy

being obtained by having a layer of a heat-insulating material at least partly surrounding the battery.

- 3. A method according to claim 2, wherein the heat-generated energy is supplied to the battery in addition to the energy supplied to the battery by the charging current so as to maintain the outer temperature of the battery within a predetermined range during a major part of the charging process.
- 4. A method according to any of claims 1-3, wherein the battery is at least partly surrounded by a layer of a heat-conductive material.
- 5. A method according to any of claims 1-4, wherein the battery and/or the heat-conductive layer is/are at least partly surrounded by a layer of a heat-insulating material.

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6. A method according to any of the preceding claims, wherein heat-generated energy is delivered to the battery so as to obtain an outer temperature of the battery within the predetermined range during the initial phase of the charging process or prior to initiating the charging process.

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- 7. A method according to any of claims 1 or 4-6, wherein the battery is a lithium battery, such as a lithium ion battery.
- 8. A method according to any of the preceding claims, wherein the predetermined range of the battery temperature is 30-60
 10 °C, preferably of 40-50 °C, and more preferred in the range of 41-46 °C.
- 9. A method according to any of the preceding claims, wherein the battery comprises at least two cells, the temperature of the battery being controlled so that the outer temperature of each cell is maintained mainly at the same value.
 - 10. A method according to any of the preceding claims, wherein the battery is packed in a battery pack, the outer temperature of the battery being obtained by supplying heatgenerated energy to the battery pack.
- 20 11. A method according to claim 10, wherein the energy is supplied by supplying an electric current to an electric circuitry or component arranged within the battery pack, said electric circuitry or component being heated by the current supplied.
- 25 12. A method according to claim 11, wherein the electric circuitry comprises one or more resistors.
- 13. A method according to any of the preceding claims, wherein the battery is a battery pack comprising at least two battery cells, and wherein the battery is charged using a voltage-balanced charging process so that the voltage of each cell is about to reach the same maximum cell voltage.

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14. A method according to claim 13, wherein the balanced charging process comprises

determining or measuring the voltage of each cell at several points in time during charging,

comparing the cell voltages measured,

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controlling the charging current of each cell so as to maintain the voltage of each cell mainly equal during a major part of the charging process.

- 15. A method according to claim 13 or 14, wherein a first
 cell having a measured first cell voltage larger than a
 measured second cell voltage of a second cell at a measurement point of time is being discharged for a period of time
 in order to lower the first cell voltage to a level mainly
 equal to the second cell voltage by controlling the balanced
 charging process.
 - 16. A method according to any of the claims 13-15, wherein the balanced charging process is controlled by an electrically balanced charging circuitry with at least part of the balanced charging circuitry being arranged within the battery pack.
 - 17. A method according to claims 11 and 16, wherein the part of the balanced charging circuitry arranged within the battery pack is heated by a current controlled by the balanced charging circuitry during said charging and/or discharging process or processes.
 - 18. A method according to claim 17, wherein a plurality of by-pass devices, one for each cell, is provided within the battery pack, said by-pass devices being used for by-passing charging current around at least one cell during said balanced charging process, said heating current comprising the by-passed charging current.
 - 19. A method according to claim 18, wherein at least one of the by-pass devices is further being supplied with a dis-

charging current when discharging one of the cells during said charging process.

- 20. A method according to claim 18 or 19, wherein electric energy is delivered to heat the battery pack through at least one electric component, in addition to one of the by-pass devices, when the heat generated by internal heating of the cells during charging and/or the by-passed current is insufficient to maintain a predetermined inner temperature of the battery pack.
- 10 21. A method of discharging a rechargeable battery comprising the steps of

withdrawing electrical energy from the battery for discharging the same, and

supplying heat-generated energy to the battery so as to increase the outer temperature of the battery during at least part of the discharging process.

22. A method according to claim 21, wherein at least part of the heat-generated energy is supplied by spontaneous heating or internal heating of the battery during the discharging process.

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23. A method of discharging a rechargeable battery comprising the steps of

withdrawing electrical energy from the battery for discharging the same, and

- 25 increasing the temperature of the battery during at least part of the discharging process by heat-generated energy due to spontaneous heating of the battery during the discharging process.
- 24. A method of discharging a rechargeable lithium ion bat-30 tery comprising the steps of

withdrawing electrical energy from the battery for discharging the same, and

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increasing the temperature of the battery during at least part of the discharging process by reducing losses in heat-generated energy due to spontaneous heating of the battery during the discharging process, said reduction in loss of energy being obtained by having a layer of a heat-insulating material at least partly surrounding the battery.

- 25. A method according to any of the claims 21-24, wherein the battery is at least partly surrounded by a layer of a heat-conductive material.
- 10 26. A method according to any of the claims 21-25, wherein the battery and/or the heat-conductive layer is/are at least partly surrounded by a layer of a heat-insulating material.
- 27. A method according to any of the claims 21-26, wherein the battery is packed in a battery pack, and the increase in the outer temperature of the battery is obtained during at least part of the discharging process by feeding current from the battery to an electric circuitry or component being arranged within the battery pack, said circuitry or component being heated by the supplied current.
- 28. A method according to any of the claims 21-27, wherein the battery is packed in a battery pack and the increase in the outer temperature of the battery is obtained before the initiation of the discharging process by feeding current from an external current source to an electric circuitry or component being arranged within the battery pack, said circuitry or component being heated by the supplied current.
 - 29. A method according to any of the claims 21-23 or 25-28, wherein the battery is a lithium battery, such as a lithium ion battery.
- 30 30. A battery system comprising a battery pack with one or more battery cells forming a rechargeable battery, said battery pack comprising

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a layer of a heat-insulating material at least partly surrounding the battery so as to maintain within the battery pack at least part of the energy generated by spontaneous heating or internal heating of the battery during discharging or charging.

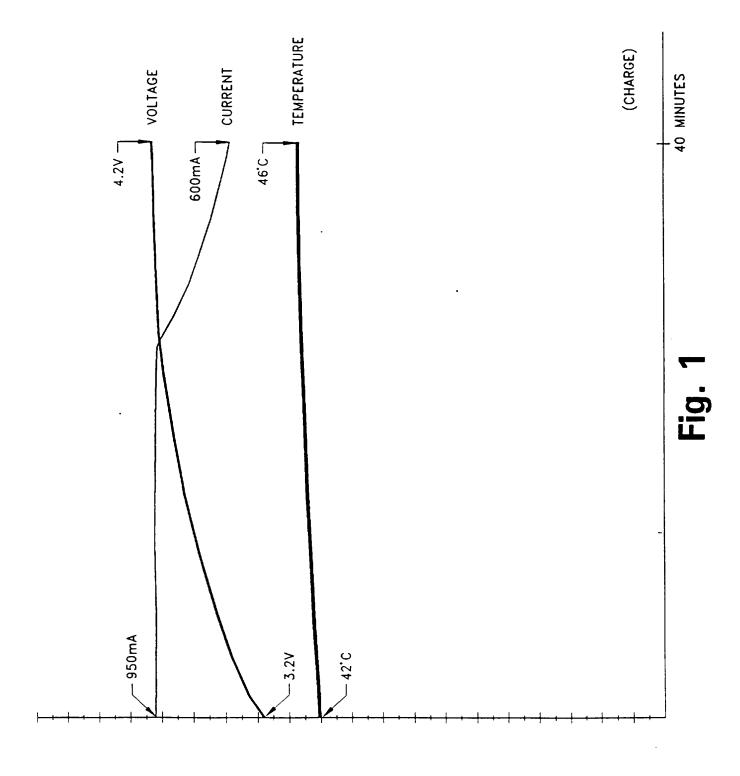
- 31. A battery system according to claim 30, further comprising a heat-conductive material arranged between the battery cells and the heat-insulating layer, and at least partly surrounding the battery cell or cells.
- 10 32. A battery system according to claim 30 or 31, further comprising an electric circuitry or component adapted to supply electric energy in the form of current-generated heat to the battery pack so as to rise the outer temperature of the battery cell or cells when said energy is supplied.
- 15 33. A battery system according to claim 32, wherein the electric circuitry comprises at least part of a battery charging system arranged within the battery pack, said part of the charging system comprising one or more by-pass devices being adapted to by-pass charging current supplied by the charging system to at least one battery cell during a charging process.
 - 34. A battery system according to claim 33, wherein the electric circuitry further comprises at least one electric component in addition to said by-pass devices, said component being arranged within the battery pack and being adapted to deliver current generated heat to the battery pack when the heat generated by the by-pass devices and/or by spontaneous heating is insufficient to maintain the outer temperature of the battery within a predetermined temperature range.
- 30 35. A battery system according to claim 33 or 34, wherein the battery charging system is adapted to by-pass the charging current around one of the battery cells when a voltage

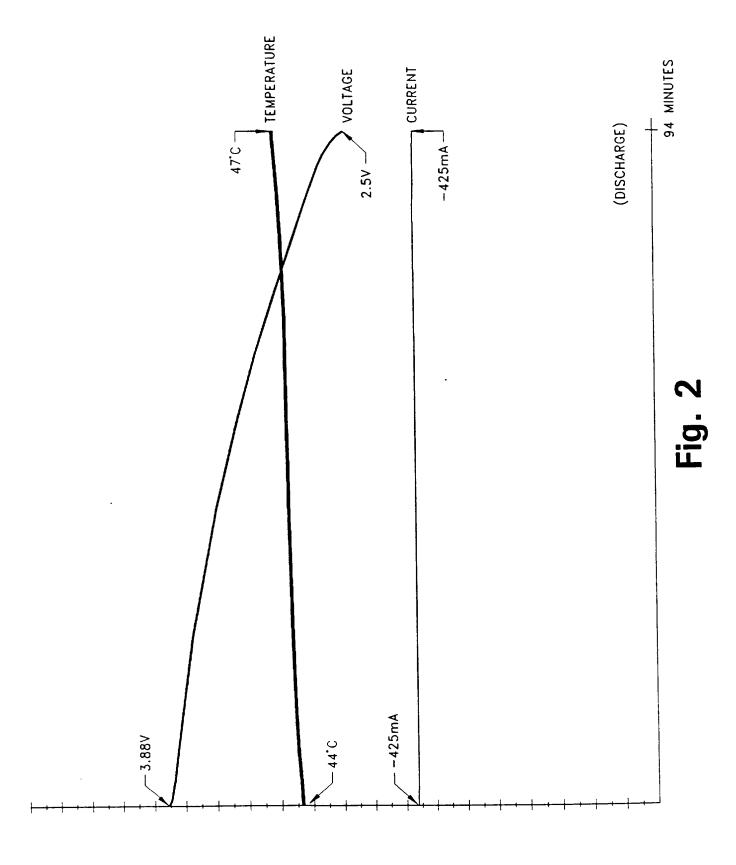
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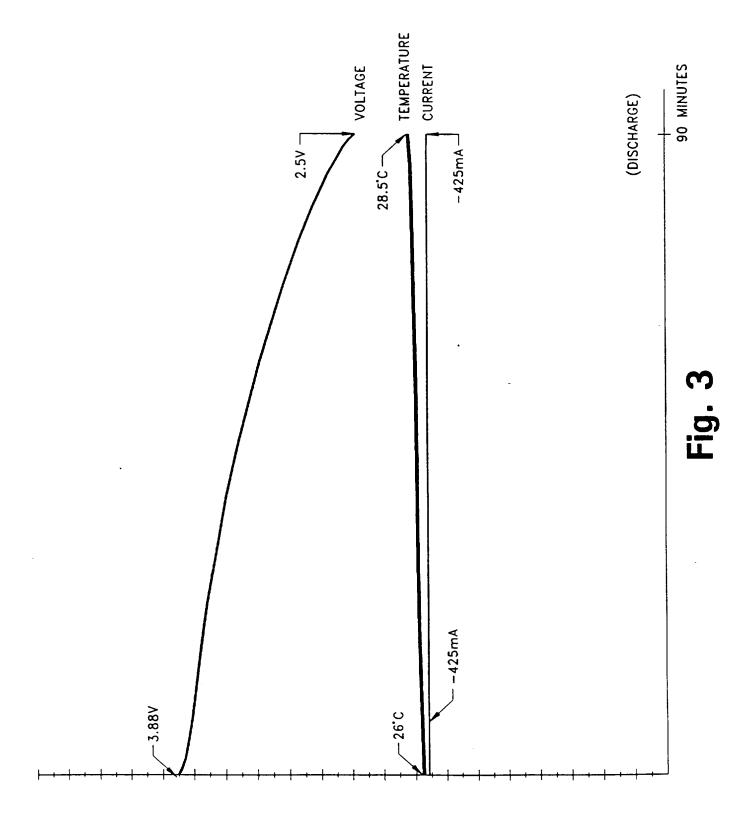
measured across said one battery cell is equal to or larger than a pre-selected maximum cell voltage.

36. A battery system according to any of the claims 30-35, wherein the battery comprises one or more lithium cells, such as lithium ion cells.

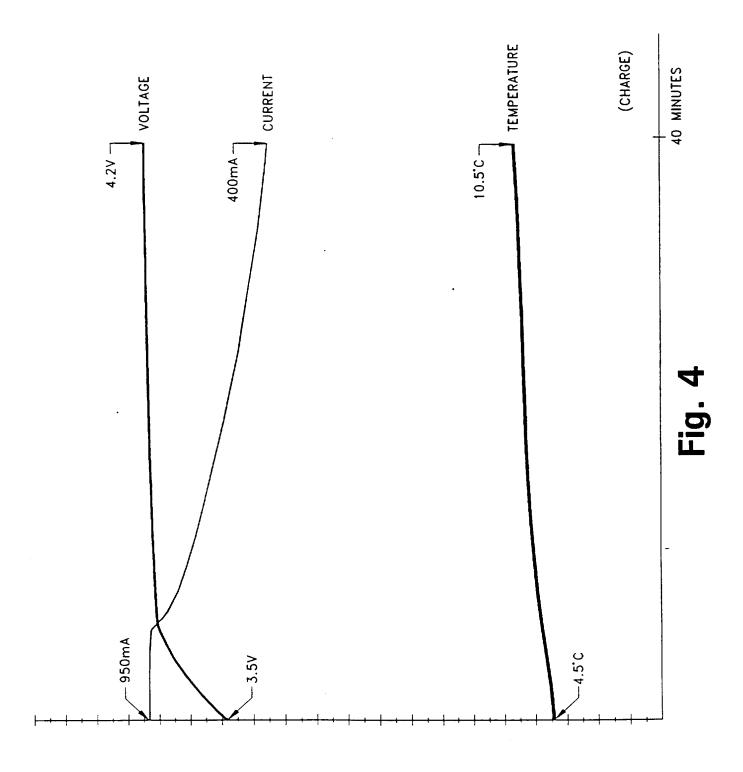




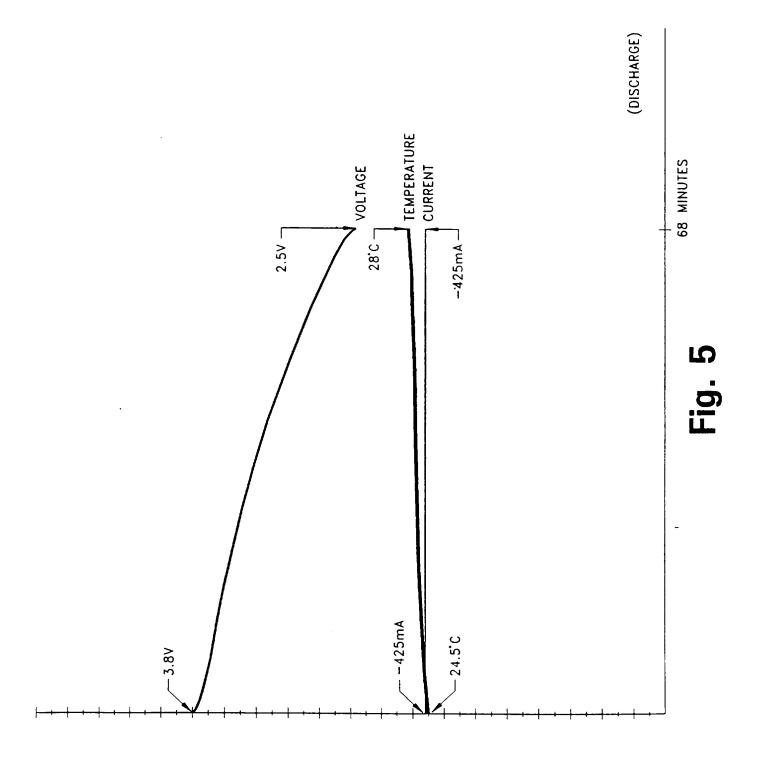
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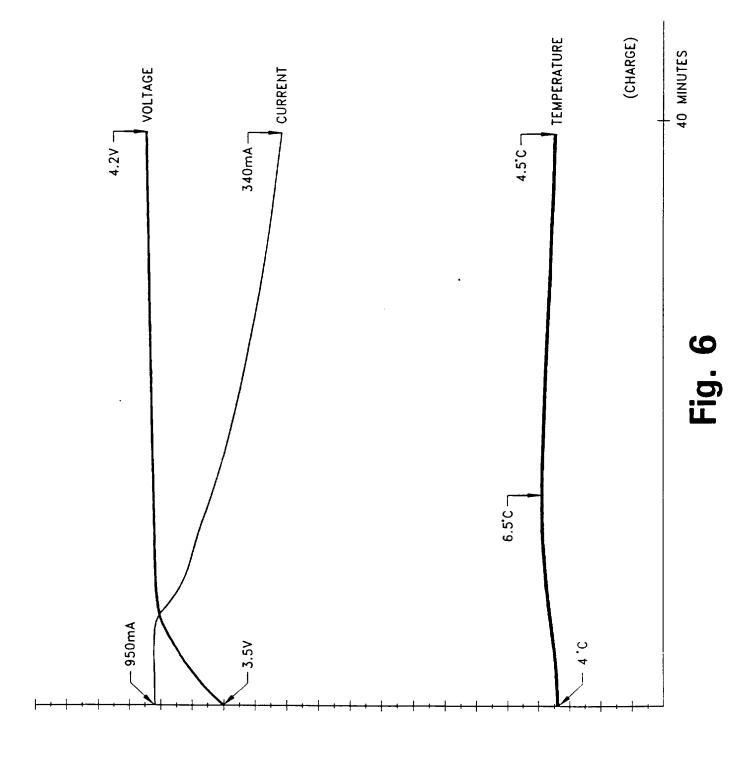
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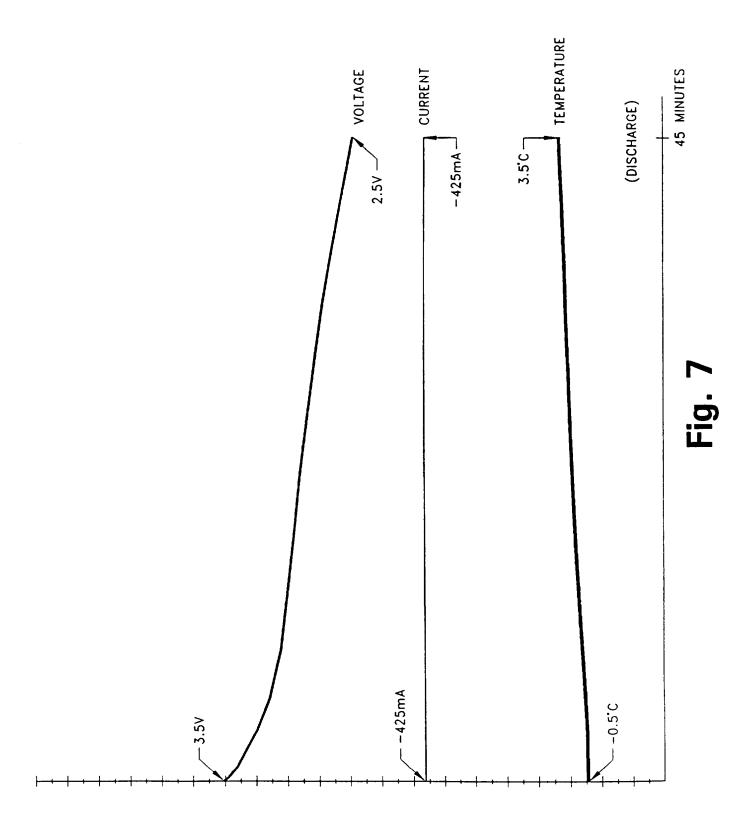
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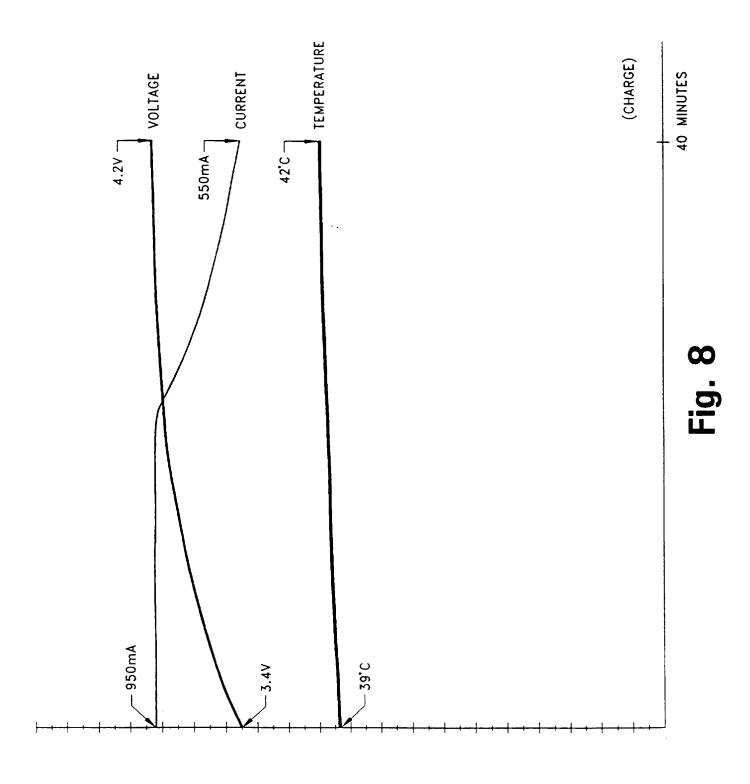
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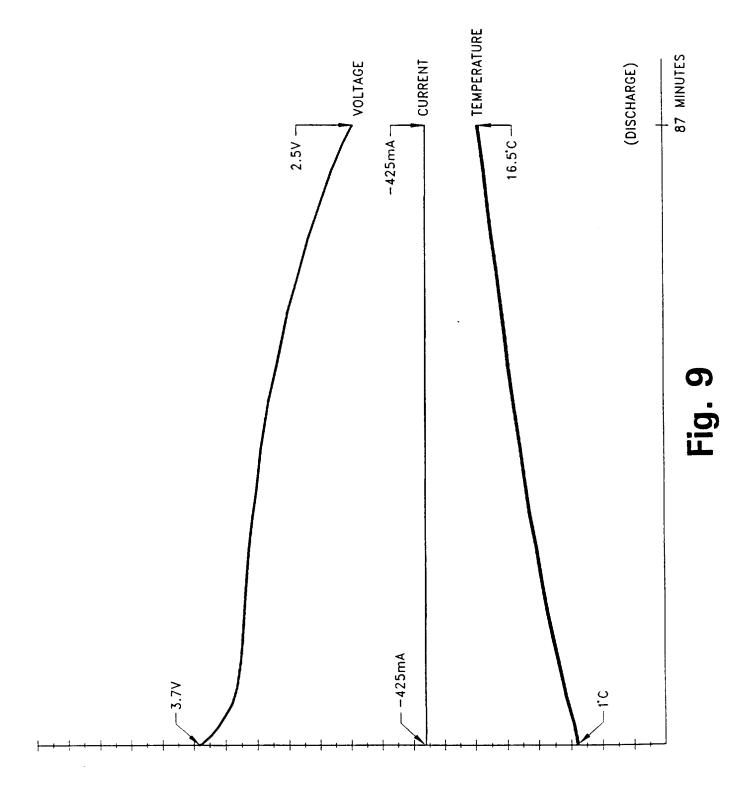


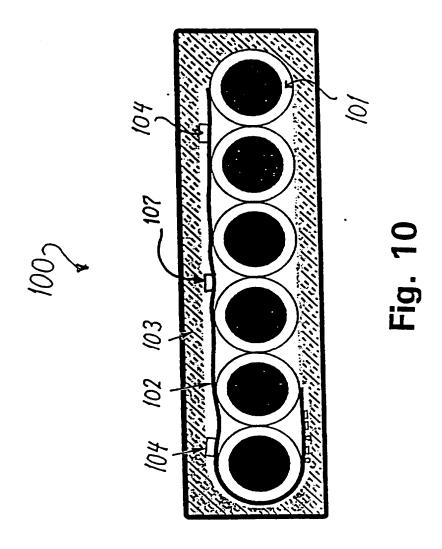
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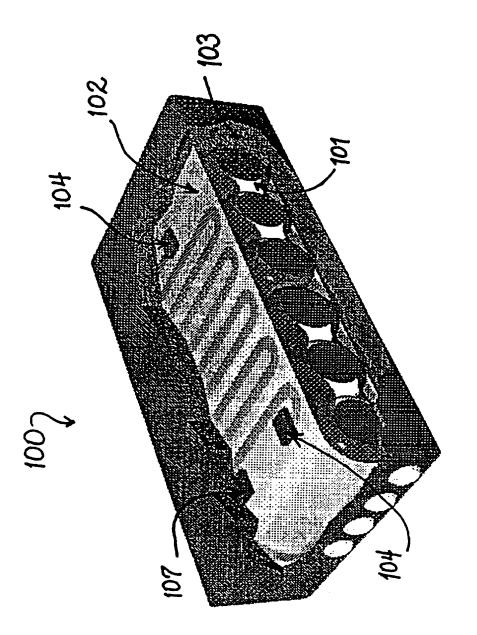


Fig. 10A

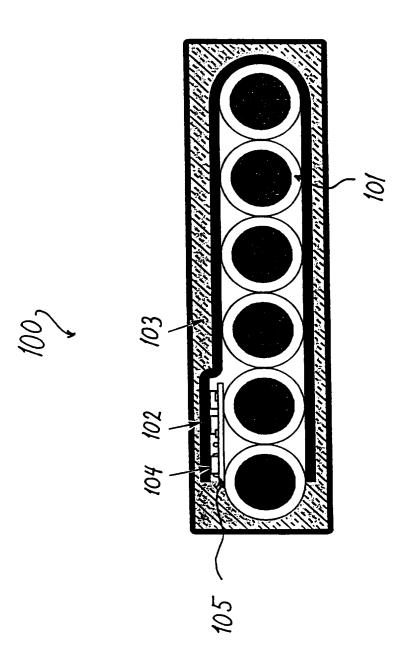
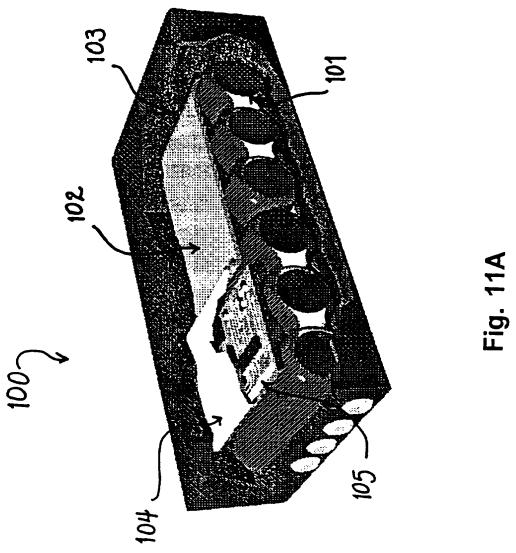
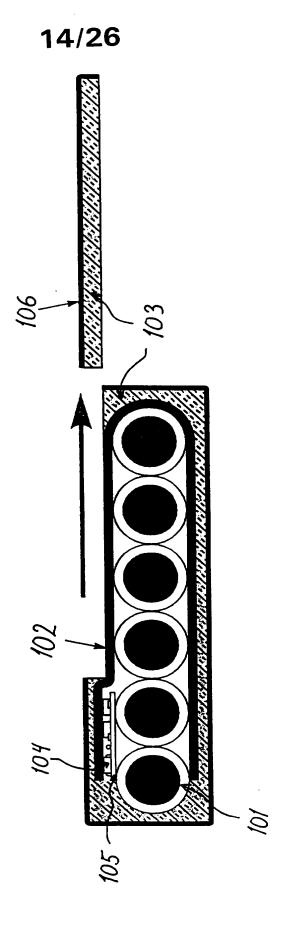


Fig. 11







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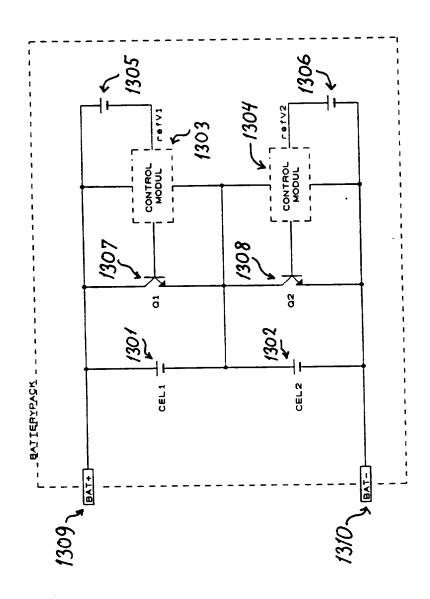
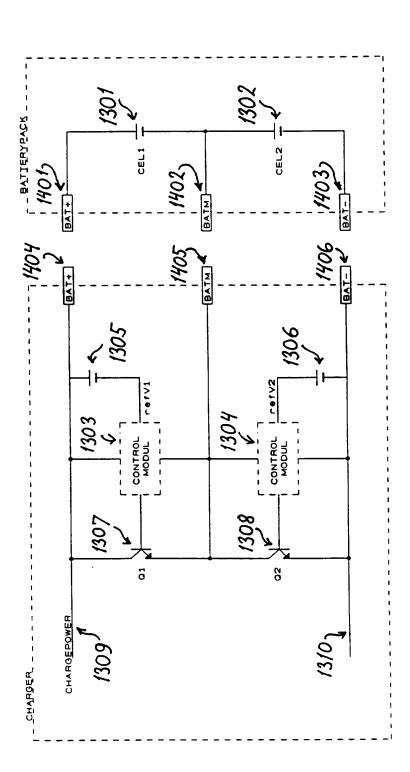


Fig. 13

Fig. 14



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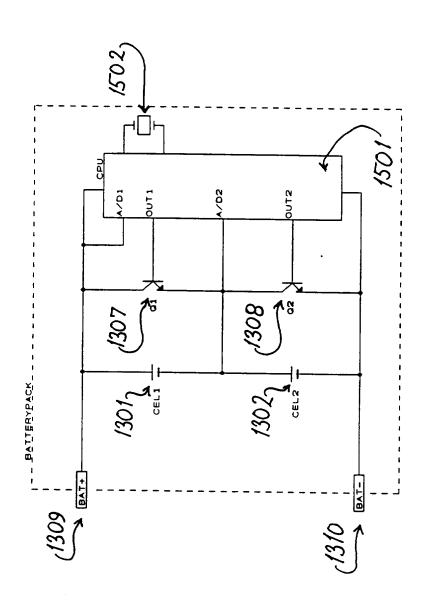


Fig. 15

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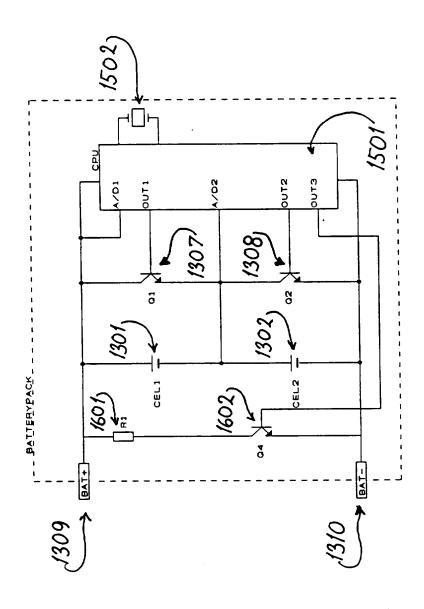


Fig. 16

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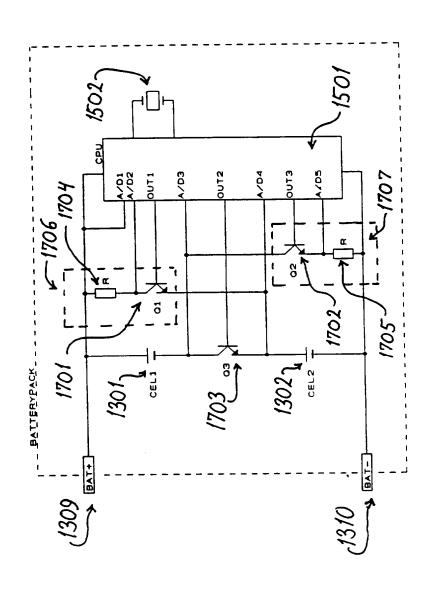
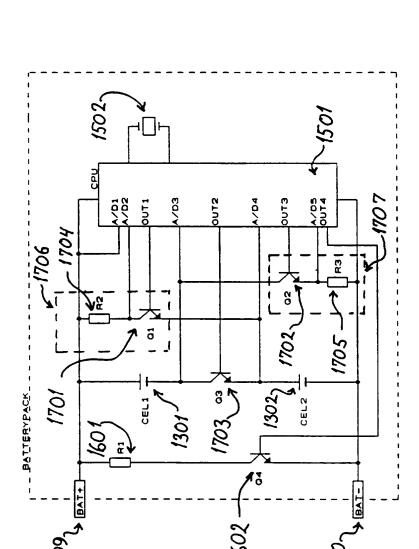


Fig. 17

Fig. 18



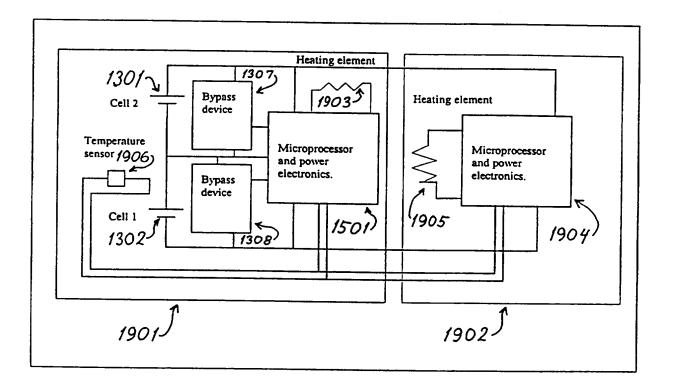


Fig. 19

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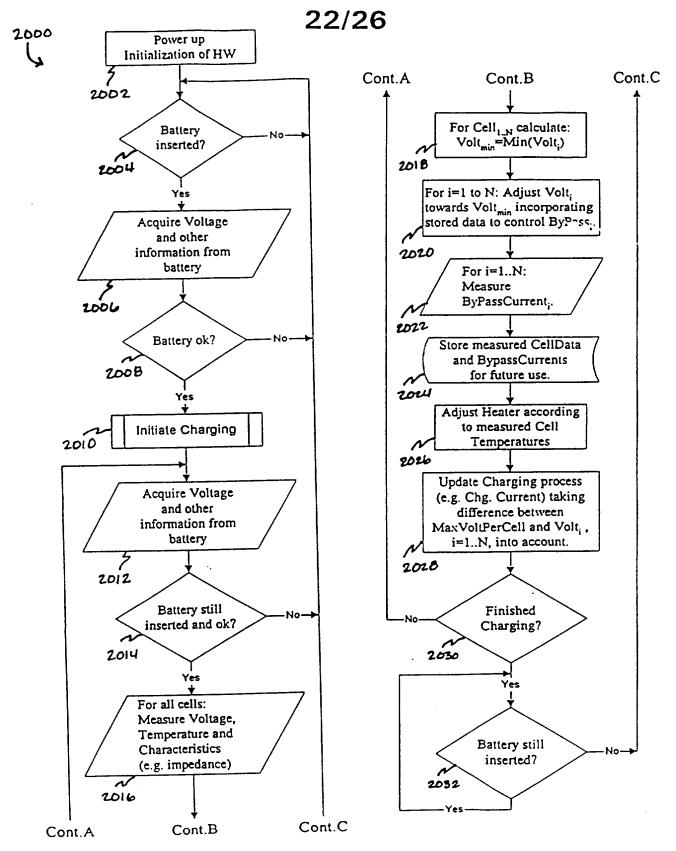


Fig. 20

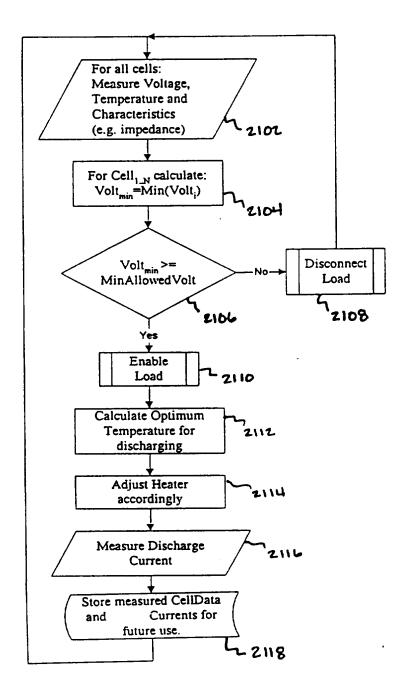


Fig. 21

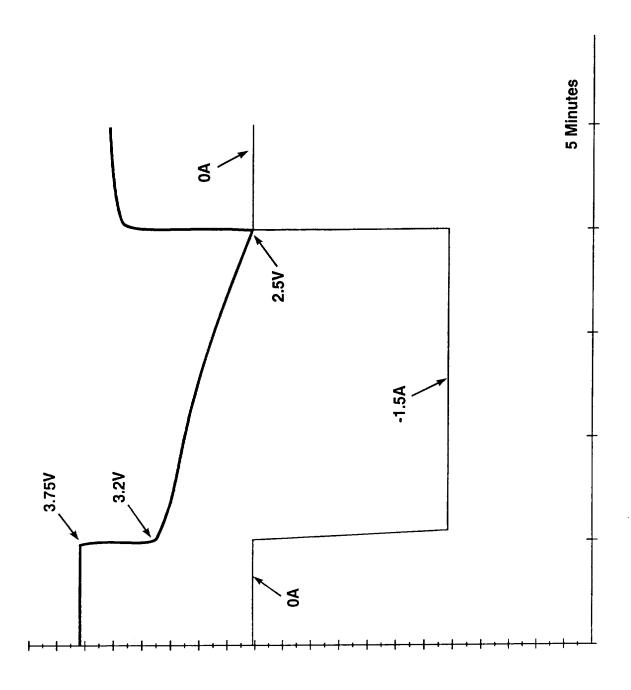


Fig. 22

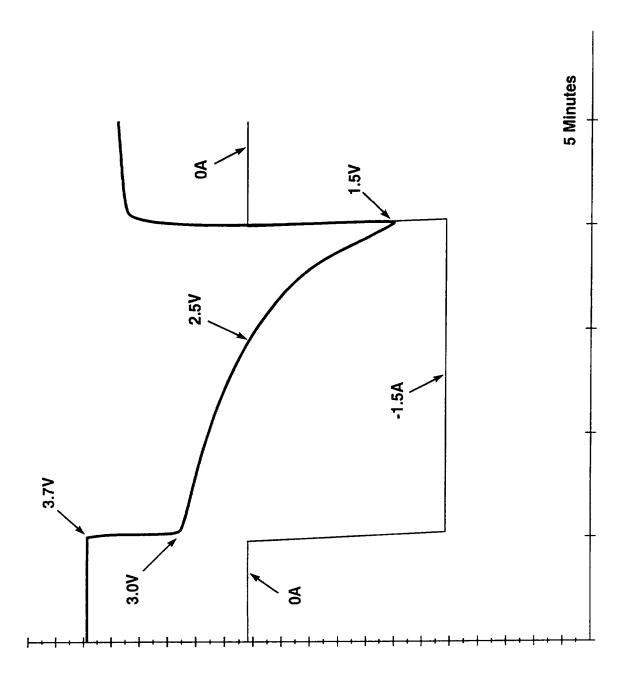


Fig. 23

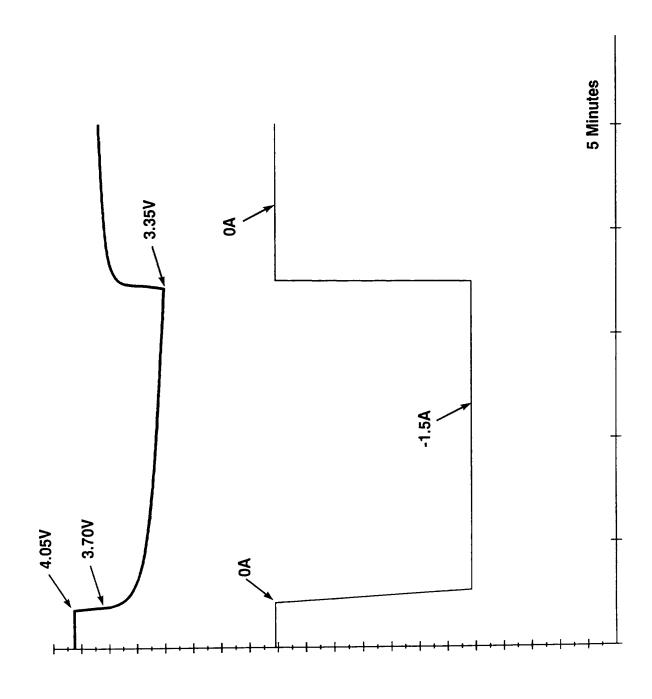


Fig. 24

Application No Internati PCT/DK 95/00477

A. CLASSIFICATION OF SUBJECT MATTER IPC 6 H01M10/50 H01M10/44
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According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) IPC 6 - H01M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

Category *	ENTS CONSIDERED TO BE RELEVANT Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Κ	DE,A,36 20 041 (LICENTIA PATENT-VERWALTUNGS GMBH) 17 December 1987	1,8-12
1	see the whole document	13,14,16
x	US,A,4 416 000 (S. SCHERBATSKOY) 15 November 1983	1-3,5-7, 10-12, 21-24, 26-30, 32,36
Y	see abstract see column 3, line 24 - line 68; figure 2	4,25,31, 33
	-/	

X Further documents are listed in the continuation of box C.	X Patent family members are listed in annex.
 Special categories of cited documents: 'A' document defining the general state of the art which is not considered to be of particular relevance 'E' earlier document but published on or after the international filing date 'L' document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) 'O' document referring to an oral disclosure, use, exhibition or other means 'P' document published prior to the international filing date but later than the priority date claimed 	 'T' later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention 'X' document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. '&' document member of the same patent family
Date of the actual completion of the international search 5 March 1996	Date of mailing of the international search report 1 0. 04. 96
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo ni, Fax: (+31-70) 340-3016	Authorized officer Helot, H

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		PCT/DK 95/00477		
C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT				
ategory °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.		
X	ELEKTROTECHNISCHE ZEITSCHRIFT - ETZ, vol. 106, no. 11, June 1985, BERLIN DE, pages 552-558, XP002000046 G.LOOCKE ET AL: "Induktive Beheizung von Kraftfahrzeug-Startbatterien" see page 554, left-hand column, line 10 - page 557, left-hand column, line 31	1,21,22		
'	US,A,4 585 712 (R. WEDLAKE) 29 April 1986 see abstract see column 4, line 15 - line 34; figures 1,2	4,25,31		
Υ	DE,A,40 17 475 (STANDARD ELEKTRIK LORENZ) 5 December 1991 see column 1, line 56 - line 62	4,25,31		
Y	EP,A,O 512 340 (SONY) 11 November 1992 cited in the application see column 1, line 7 - line 29	7,29,36		
Y	W0,A,89 09497 (SECR DEFENCE BRIT) 5 October 1989 see abstract see page 2, line 1 - line 28 see page 3, line 2 - page 4, line 25; figure 1	7,29,36		
Y	DE,A,40 27 149 (BEHNISH J) 28 March 1991 see column 1, line 55 - line 63	16,34		
Y A	US,A,4 238 721 (W.DELUCA ET AL) 9 December 1980 see column 4, line 20 - column 6, line 1	13,14, 16,33,34 18,19		
A	CH,A,662 448 (KERN) 30 September 1987 see the whole document	13,14		
A	DE,A,25 59 364 (MAXS AG) 14 July 1977 see page 11, line 5 - page 14, line 9	13-15		

1

Internat Application No
PCT/DK 95/00477

			PC1/UN	
Patent document ited in search report	Publication date 17-12-87 15-11-83	Patent family member(s)		Publication date
DE-A-3620041		NONE		
S-A-4416000		AU-B- CA-A- CA-A- CA-A- CA-A- DE-A-	4134478 1124228 1150716 1145323 1166626 2852575	14-06-79 25-05-82 26-07-83 26-04-83 01-05-84 07-06-79
		FR-A,B GB-A,B GB-A,B GB-A,B	2410726 2009473 2096372 2096373 2094527 2094528	29-06-79 13-06-79 13-10-82 13-10-82 15-09-82 15-09-82
		GB-A,B NL-A- SU-A- US-A- US-A-	7811317 1243633 5390153 4351037	07-06-79 07-07-86 14-02-95 21-09-82 12-09-89
		US-A- US-A- US-A- US-A-	4866680 4839870 5150333 4520468 5113379 5079750	13-06-89 22-09-92 28-05-85 12-05-92 07-01-92
		US-A- US-A- US-A-	5182730 4692911	26-01-93 08-09-87
US-A-4585712	29-04-86	DE-A- FR-A,B GB-A,B JP-B- JP-A-	3501824 2558650 2153136 8001815 60163386	25-07-85 26-07-85 14-08-85 10-01-96 26-08-85
DE-A-4017475	05-12-91	AU-B- AU-B-	650015 7719091	09-06-94 05-12-91
EP-A-0512340	11-11-92	JP-A- US-A-	4331425 5304915	19-11-92 19-04-94
WO-A-8909497	05-10-89	EP-A-	0406295	09-01-91

Internat Application No
PCT/DK 95/00477

Patent document cited in search report	Publication date	Patent family member(s)		Publication date	
WO-A-8909497		GB-A-	2234625	06-02-91	
DE-A-4027149	28-03-91	CA-A-	2050071	01-03-92	
US-A-4238721	09-12-80	NONE			
CH-A-662448	30-09-87	NONE			
DE-A-2559364	14-07-77	NONE			